

# Scaling Models for the Refractive Index of HFC 134a and HFC 143a on the Coexistence Curve

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## Abstract

A scaling form for the refractive index  $n$  is investigated in the work. It based on the scaling theory (ST) and experimental data on  $n_b n_g, T$  – data Yata [1,2] along the coexistence curve (CC) including a wide region around the critical point of HFC 134a and HFC 143a. A methodical part deals with an equation  $n_b n_g(T)$  that is a combination of two properties, the order parameter  $f_s$  and the diameter of CC  $f_d$ . It is accepted that the properties,  $Y = (f_s f_d)$ , have a scaling part,  $Y_{scal}$ , and a regular one,  $Y_r$ . The form of  $Y_{scal}$  has followed to the scaling theory (ST), depended on the relative distance  $\tau$  from  $T_c$  and parameters (critical exponents  $(\alpha, \beta, (\Delta_i))$  and amplitudes,  $(B_{si}), (B_{di})$ ).

A routine and some criterions are elaborated for the task: to determine parameters of  $Y$  with the help of  $n_b n_g, T$  – data. The scaling function  $\psi_{l,g}$  is used to analyze  $Y$ . With the help of the routine numerical parameters of  $n_l(\tau)$  and  $n_g(\tau)$  are calculated. They represent reliable experimental points in a region from 300 K up to  $T_c$ . The relations represented reliable measured points including new data in limits of experimental errors and can be helpful to calculate densities on CC in a wide region of the critical point,  $0.00003 < \tau < 0.2$ . The relations,  $\rho_l(T), \rho_g(T)$ , include effective values of critical exponents,  $\alpha, \beta$ . A comparison has shown that there is a

satisfy agreement the values with exponents,  $\alpha, \beta$ , those are used in scaling equations,  $\rho_l(T)$ ,  $\rho_g(T)$ .

**Keywords:** HFC 134a; HFC 143a; Thermodynamic properties; Scaling equation; Refractive index; Density of liquid, Density of vapor; Coexisting curve.

## 1. Introduction

Due to ST the properties on CC,  $\rho_l(T), \rho_g(T)$ , can be represent with the help of the order parameter  $f_s$  and the diameter of CC  $f_d$  [3,4] in some region of  $T_c$ .

$$f_s = (\rho_l - \rho_g)(2\rho_c)^{-1} = B_{s0}\tau^\beta + B_{s1}\tau^{\beta+\Delta_1} + B_{s2}\tau^{\beta+\Delta_2}, \quad (1.1)$$

$$f_d = (\rho_l + \rho_g)(2\rho_c)^{-1} - 1 = B_{d0}\tau^{1-\alpha} + B_{d1}\tau^{1-\alpha+\Delta_1} + B_{d2}\tau^{1-\alpha+\Delta_2}. \quad (1.2)$$

The first addend in (1.1) (1.2) represents the asymptotic component, the second and the third terms give non asymptotic components (the first and the second correction terms with correction exponents  $\Delta_1$  and  $\Delta_2$ ).

Analytic equations,  $\rho_l(T), \rho_g(T)$ , can be determined with the help of known (1.1,1.2) as

$$\rho_l = (f_d + f_s + 1) \rho_c, \quad \rho_g = (f_d - f_s + 1) \rho_c. \quad (1.3)$$

Equations (1.1,1.2) are named Model 1, they can approximate experimental data in a working interval  $\Delta \tau_w \approx 0.15$  of  $T_c$  ( $T_c > T > T_w$ ,  $\Delta \tau_w = 1 - T_w/T_c$ ) for different substances. RMS deviations,  $S_g, S_l$ , are small and no systematic deviations are realized. Our practice showed if  $T_w$  decreases and  $\Delta \tau_w > 0.1$  then RMS deviations,  $S_g, S_l$ , increase and remarkable systematic errors appear. A combined model named Model 2 is proposed for the case in [3,4].

We have decided to choose an analogous form for representation of  $n_{l,g}(\tau)$  equation.

## 2. Models, criterions and routines

To represent  $n_l, n_g, T$  – data in  $\Delta \tau_w > 0.1$  we have taken Model 2 adopted to  $n_{l,g}(\tau)$

$$f_s = (n_l - n_g)(2n_c)^{-1} = B_{s0}\tau^\beta + B_{s1}\tau^{\beta+\Delta_1} + B_{s2}\tau^{\beta+\Delta_2} + B_{s3}\tau^2 + B_{s4}\tau^3, \quad (2.1)$$

$$f_d = (n_l + n_g)(2n_c)^{-1} = B_{d0}\tau^{1-\alpha} + B_{d1}\tau^{1-\alpha+\Delta_1} + B_{d2}\tau^{1-\alpha+\Delta_2} + B_{d3}\tau^2 + B_{d4}\tau^3. \quad (2.2)$$

Analytic equations,  $\rho_l(T), \rho_g(T)$ , can be determined with the help of known (2.1,2.2) as

$$\rho_l = (f_d + f_s + 1) \rho_c, \quad \rho_g = (f_d - f_s + 1) \rho_c. \quad (2.3)$$

Two regular terms in (2.1,2.2) are involved with the aim to reduce possible systematic deviations mentioned for Model 1 under  $\tau_w > 0.1$ . Model 2 is to have the following characteristics: 1) it approximates  $n_i, n_g, T$  – data in  $\Delta\tau_w > 0.1$  with acceptable RMS deviations,  $S_g, S_l$ , 2) at the same time its scaling part (it can be consider as Model 1) delivers acceptable RMS deviations,  $S_g, S_l$ , for points in  $\Delta\tau_w = 0.1$  when Model 1 is used to calculate deviations of  $\rho_i, \rho_g, T$  – data in  $\Delta\tau_w = 0.1$ . In the case the regular terms play a role of correction addends:  $S_l(\text{Model 1}) \approx S_l(\text{Model 2})$  and  $S_g(\text{Model 1}) \approx S_g(\text{Model 2})$ .

An approximation quality of Model 2 is characterized by individual and RMS deviations of experimental ( $n_{g \exp k}, n_{l \exp k}$ ) values from those calculated with equations (2.3)

$$\begin{aligned} \delta\rho_{gk} &= 100 (\rho_{g \exp k} - \rho_{gk}) / \rho_{gk}, & S_g &= (\sum \delta\rho_{gk}^2 / N)^{0.5}, \\ \delta\rho_{lk} &= 100 (\rho_{l \exp k} - \rho_{lk}) / \rho_{lk}, & S_l &= (\sum \delta\rho_{lk}^2 / N)^{0.5}, \end{aligned} \quad (2.4)$$

Model 2 can be considered as  $Y = (f_s, f_d)$  that includes parameters,  $D = (\rho_c, T_c, \alpha, \beta, (\Delta_i))$ , and coefficients,  $C = ((B_{si}), (B_{di}))$ . Values of  $C$  are to be determined by an approximation of the input data set ( $Y_{\exp k}, \tau_k$ ). If  $D$  are considered as the parameters fixed and known (taken from literature sources) then  $Y = f(D, C, \tau)$  is a linear function of  $C$ . In the case it is possible to calculate  $C$  using a weighted least-squares analysis (LSQA) and a single criterion – a minim of the functional  $\Phi(C, D)$

$$\Phi(C, D) = \sum_{k=1}^N w_k (Y_{\exp k} - f(D, C, \tau_k))^2 / N = \min. \quad (2.5)$$

Routine 1 is elaborated for  $C$  calculation and has the following steps: i) to consider  $D$  as the parameters fixed and to take from literature sources; ii) to form a sum of squares,  $\Phi(C, D)$ , for the input data set; iii) to calculate a realization  $C$ , that is numerical values of  $C$ , using a weighted least-squares analysis (LSQA) and a single criterion – a minim of  $\Phi(C, D)$ ; ii) to estimate a quality of the approximation that is to calculate individual and RMS deviations .

Routine 1 was used and gave an opportunity to examine a group of realizations ( $Y = f(D_j, C_j, \tau)$ ,  $j = 1 \dots K$ ). Criterion (1.6) shows that  $\Phi(C, D)$   $S_{l,g}(D)$  are some functions of parameters

*D.* If Routine 1 is used at the first time then the following numerical values appear: parameters,  $D = D_1$ , a realization,  $C = C_1$ , RMS deviations,  $S_{l,g}(D_1)$ . If one of the parameters  $D_1$  is shifted (for example  $\rho_c$  can be shifted on  $\Delta\rho_c$  in limits of an experimental estimation  $\pm\Delta\rho_c$ ) then Routine 1 can be used at the second time and the second set,  $D_2, C_2, S_{l,g}(D_2)$ , can be got. Many numerical variants (realizations ( $C_j$ )) of Models 1,2 and according deviation sets ( $S_{l,g}(D_j)$ ) were got, among them there were such numerical dependences as  $S_{l,g}(n_c), S_{l,g}(T_c), S_{l,g}(\beta)$  in some region of  $S_l^{min}$  and  $S_g^{min}$ . Our analyses have estimated some general features of the realisations: i) values of  $S_g$  and  $S_l$  did not coincide ( $S_l < S_g$ ), the global minimal values were found between them (Model 2 has given  $S_l^{min} = 0.01\%$  and  $S_g^{min} = 0.005\%$  for HFC 134a points related to  $\Delta\tau_w = 0.25$ , ii) the leading amplitudes,  $B_{s0}, B_{d0}$ , deviated greatly from middle calculated values,  $B_{s0}, B_{d0}$ , iii) it was impossible to find a variant  $C_j$  that delivered  $S_l = S_l^{min}$  and  $S_g = S_g^{min}$  at once. The last circumstance was one of the reasons to look for an optimal Models 1,2 ( $Y = f(D_{opt}, C_{opt}, \tau)$ ) with an optimal realization  $C_{opt}$  that deliver compromise values of  $S_{l,g}(D_{opt})$ . It was admitted that the realization  $Y = f(D_{opt}, C_{opt}, \tau)$  is optimal when  $Y$  deliver RMS deviations those follow to the compromise criterions

$$S_l(D_j) - S_l^{min} < \varepsilon_1, \quad S_g(D_j) - S_g^{min} < \varepsilon_2, \quad (2.6)$$

where  $\varepsilon_1$  and  $\varepsilon_2$  – some limits.

Our practice and analysis of realizations, ( $Y_j$ ), have showed that more criterions have to be involved for the purpose to choose an optimal variant from realizations ( $Y_j$ ) those satisfied criterions (2.6). One more property is considered in ST and involved in the work: the scaling function  $\psi_{l,g}$  that can be expressed in the form

$$\psi_{l,g} = |(n_{l,g} - n_c)(2n_c \tau^\beta)^{-1}| = |\pm B_{s0} + B_{d0} \tau^{1-\alpha-\beta} \pm B_{s1} \tau^{\Delta 1-\beta} + B_{d1} \tau^{1-\alpha+\Delta 1-\beta} + \dots|, \quad (2.7)$$

where the upper (plus) sign of terms corresponds to the liquid branch (*l*), the lower (minus) corresponds to the vapor branch (*g*) of  $\psi_{l,g}$ .

Investigations [3,4,5] estimated that the scaling function  $\psi_{l,g}$  can be used as an additional criterion.  $\psi_{l,g}$  is written in a narrow interval  $\tau_w \approx 0.01$  as two terms expression that includes only leading addends with the asymptotic exponents

$$\psi_{l,g} \approx |\pm B_{s0} + B_{d0} \tau^{1-\alpha-\beta}|. \quad (2.8)$$

A numerical form (2.8) of  $\psi_{l,g}$  was found and analysed for several liquids ( $H_2O, Ne, N_2, HFC$  134a,  $HFC$  143a a. o.). Due to (2.8) an optimal variant,  $Y = f(D_{opt}, C_{opt}, \tau)$ , is to follow to the next features: i)  $\psi_{l,g}$  is symmetric to the amplitude  $B_{s0}$  for liquid and vapour branches, ii) the plot of  $\psi_{l,g}$  versus  $\tau^{1-\alpha-\beta}$  is liner and converge symmetrically to  $B_{s0}$ , iii) asymptotic Model 0 as  $Y = f(D_{opt}, C = B_{s0}, B_{d0}, \tau)$  can be built, optimal Model 0 is to have a satisfied agreement with experimental points related to  $\tau_w \approx 0.01$ , RMS deviations,  $S_b, S_g$ , are close to criterions (2.6) in the case. An illustration of  $\psi_{l,g}$  as a function of  $\tau^{1-\alpha-\beta}$  is given in Fig. 1,2. Experimental values of  $\psi_{l,g}$  are shown as well as values determined with the help of Models 0,1,2 for  $HFC$  134a. Two methods of parameters  $D$  chose were examined for the task. Due to the first one  $D$  components are taken as theoretical or experimental values and not varied during a treaty of the input data set. For example the exponents are taken in [2] as theoretical data  $\beta=0.325$ ,  $\alpha=0.1085$  and  $\Delta=0.5$  for the densities equations,  $\rho_l(T), \rho_g(T)$ . We have used the way for  $(\Delta_i)$  determination and chosen  $\Delta_1 = \Delta = 0.5$  and  $\Delta_2 = 2\Delta$  as theoretical values. The second method [3 - 6] considers  $D = (\rho_c, T_c, \alpha, \beta, B_{s0}, B_{d0})$  as fixed parameters for the densities equations,  $\rho_l(T), \rho_g(T)$ ;  $D$  is known in a region of possible deviations  $(\pm \Delta D)$  and the method let us i) shift  $D$  in the limits  $(\pm \Delta D)$  corresponding to some criterions, ii) examine a group  $(D_j)$  and choose an optimal variant. We underline that leading amplitudes,  $B_{s0}, B_{d0}$ , are also included in  $D$  and they do not take part in LSQA when amplitudes  $C$  are determined. This schema has been accepted in the work.

The middle value of  $D$  components and a region of possible deviation  $(\pm \Delta_{\rho_c}, \pm \Delta_{T_c}, \pm \Delta_{\beta}$  a.o.) were found among parameters of realization,  $(Y_j)$ , calculated during the investigation. The start values were chosen:  $\alpha=0.1085$  and  $\beta=0.325$ ,  $T_c = 374.107 \pm 0.02$  K [1],  $n_c = 1.08990$  [1]. The

characteristics were combined in a group  $D_1 = (n_c, T_c, \alpha, \beta, \Delta B_{s0}, B_{d0})$  as a start data. The value  $\beta = 0.348 \pm 0.001$  was reported by Yata [1] as an effective exponent got from  $\rho_l, \rho_g, T$  – data. The region was also used in Routine 2.

Routine 2 was elaborated using criterions (2.6,2.8). It consisted of several steps: i) to take  $D_1$  as start fixed parameters, ii) to calculate the realization  $C_1$  employing weighted LSQA, iii) to determine the criterions  $(S_l, S_g, \psi_{l,g})$  and to analyse them; if the analysis showed that criterions  $(S_l, S_g, \psi_{l,g})$  satisfied conditions (2.3,2.4) then the routine was to finish. On opposite site, a new fixed parameter (for example, it was  $n_c$ ) was to be chosen ( $n_c$  was shifted on  $0.1 \Delta n_c$ ),  $D_2$  was formed and treaty was continued (steps ii,iii) to get next realisation  $C_2$ . There is an illustration in Fig. 1 of a dependence,  $S_l(n_c)$ , when  $n_c$  is shifted step by step in a region,  $\Delta n_c$ , of  $S_l^{min}$ . Routine 2 builds Models 1,2 for HFC 134a when  $n_c$  increases from 1.089795 to 1.089805 with the step 0.000001 and the value of  $S_l$  changes in the interval 0.021...0.15 %. The dependence shows: if the limit is taken as  $\varepsilon_2 \approx 0.01\%$  then  $n_c$  lies in the interval  $1.089801 \pm 0.000001$ . A similar dependence is found for  $S_g(n_c)$  and  $\varepsilon_2 \approx 0.01\%$  has been accepted .

Routine 2 let us get Models 1,2 those had effective parameters,  $D_{opt}, C_{opt}$ , and were agree with conditions (2.3,2.4). The routine was used to build Model 1,2 using  $n, n_g, T$  –points of HFC 134a and HFC 143a in  $\tau_w \approx 0.2$ . The limits,  $\varepsilon_1, \varepsilon_2$ , are determined as  $\varepsilon_1 = \varepsilon_2 \approx 0.01\%$ . Numerical parameters of Model 2 are placed in tables 1,2. Model 2 was fitted to the input data set with acceptable accuracy in the gas and liquid phases. Values of  $\psi_{l,g}$  calculated with the parameters (table 1) are placed in Fig. 2,3. There are values determined with the help of Models 0,1 in Fig. 2. The models have used the parameters (Table 1) and represent scaling terms of a combined equation (2.1,2,2). In Fig. 3 there are values determined using Model 2 with the parameters (Table 1). Experimental values of  $\psi_{l,g}$  are shown too.

Following approximation characteristics,  $S_l, S_g, S_l^{min}, S_g^{min}$ , were got: for Model 1  $S_l = 0.017\%$ ,  $S_g = 0.013\%$ ,  $S_l^{min} = 0.021\%$ ,  $S_g^{min} = 0.014\%$ ; for Model 2  $S_l = 0.019\%$ ,  $S_g = 0.021\%$ ,  $S_l^{min} = 0.012\%$ ,  $S_g^{min} = 0.013\%$ .

**Table 1.** Parameters of Model 2 for HFC 134a.

$n_c$	$T_c / K$	$\alpha$	$\beta$	$\Delta$
1.089801	374.105	0.1509	0.34942	0.5
$B_{s0}$	$B_{s1}$	$B_{s2}$	$B_{s3}$	$B_{s4}$
0.1757	0.003521	-0.0369	-0.030079	0.095459
$B_{d0}$	$B_{d1}$	$B_{d2}$	$B_{d3}$	$B_{d4}$
0.06605	0.011038	0.030092	-0.000207	-0.004037

**Table 2.** Parameters of Model 2 for HFC 143a.

$n_c$	$T_c / K$	$\alpha$	$\beta$	$\Delta$
1.09125	345.815	0.22	0.3515	0.5
$B_{s0}$	$B_{s1}$	$B_{s2}$	$B_{s3}$	$B_{s4}$
0.1761	0.006851	-0.066169	0.053325	0.148388
$B_{d0}$	$B_{d1}$	$B_{d2}$	$B_{d3}$	$B_{d4}$
0.0066	0.250177	-0.326997	0.0673	0.131136

There is an illustration in Fig. 4 of a dependence,  $S_l(T_c)$ , for Modes 1,2 when  $T_c$  is shifted step by step in the interval  $\Delta T_c = 374.10...374.12$  K including the point with  $S_l^{min}$ . Routine 2 let us use the step 0.0005 ...0.001 K and estimate that  $S_l$  changes in the interval 0.021...0.35 % (Model 1) and 0.012...0.033 % (Model 2). The dependence shows: if the limit is taken as  $\epsilon_2 \approx 0.01\%$  then i)  $T_c$  can be chosen as  $T_c = 374.105 \pm 0.001$  K and ii) Models 1,2 will have the following criterions of approximation:  $S_l = 0.021...0.031$  for Model 1,  $S_l = 0.05...0.021\%$  for Model 2. A comparison shows that Models 1,2 have similar RMS deviations at  $T_c = 374.105$  K.

The equalities,  $S_l(\text{Model 1}) \approx S_l(\text{Model 2})$ ,  $S_g(\text{Model 1}) \approx S_g(\text{Model 2})$ , mean that the scaling part plays the leading role and the influence of the regular part is small in optimal variant of Model 2.

#### 4. Conclusion

The analysis of realizations, an optimal variant of Model 2 and results of a comparison with the data [1,2] allows us to make an output that the structure of Model 2 can be useful to approximate experimental data on a line of the phase equilibrium including a broad neighborhood of the critical point. Numerical variants of  $n_l(T), n_g(T)$  for HFC134a represent experimental data in the region,  $0.00003 < \tau < 0.2$ , with satisfy RMS deviations: for Model 1  $S_l = 0.017\%$ ,  $S_g = 0.013\%$ ; for Model 2  $S_l = 0.019\%$ ,  $S_g = 0.021\%$ . The Models can be used to determine accurate  $\rho_l, \rho_g T$  – data including asymptotic region of the critical point where traditional methods have a low accuracy. Effective values of critical characteristics,  $n_c, T_c, \alpha, \beta, B_{s0}, B_{d0}$ , are interesting data for problems of ST.

**Acknowledgments.** The work was supported by the Russian Fund of Base Researches.

#### *List of symbols*

$T$  = temperature

$P$  = pressure

$\rho$  = density

$P_s$  = saturated pressure

$g, l, c$  = indexes to mark the vapor and liquid phases on CC and a value in the critical point

$\alpha, \beta, (\Delta_i)$  = critical exponents

$\tau = 1 - T/T_c$  = relative distance of temperature from  $T_c$ ,

$(B_{si}), (B_{di}), (B_{pi})$  = amplitudes

$\delta\rho_{gk}, \delta\rho_{lk}$  = relative deviations of the vapour and liquid densities in  $k$  – point

$\rho_{g\ exp\ k}, \rho_{l\ exp\ k}$  = experimental values of the the densities

$\rho_{g\ k}, \rho_{l\ k}$  = values of the vapour and liquid densities calculated with (1.4)



$N$  = the number of points in the input data set

$S_g, S_l$  = relative RMS deviations of vapour and liquid densities.

$w_k$  = weight coefficient for  $k$  – point

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Fig. 1. The scaling functions  $\psi_{l,g}$  of HFC 134a.

Values are determined from 1) the experimental data, 2) Models 0,1;

$b_0$  – leading amplitude  $B_{s0}$ ; relative temperature –  $\tau^{1-\alpha-\beta} = (1 - T/T_c)^{1-\alpha-\beta}$

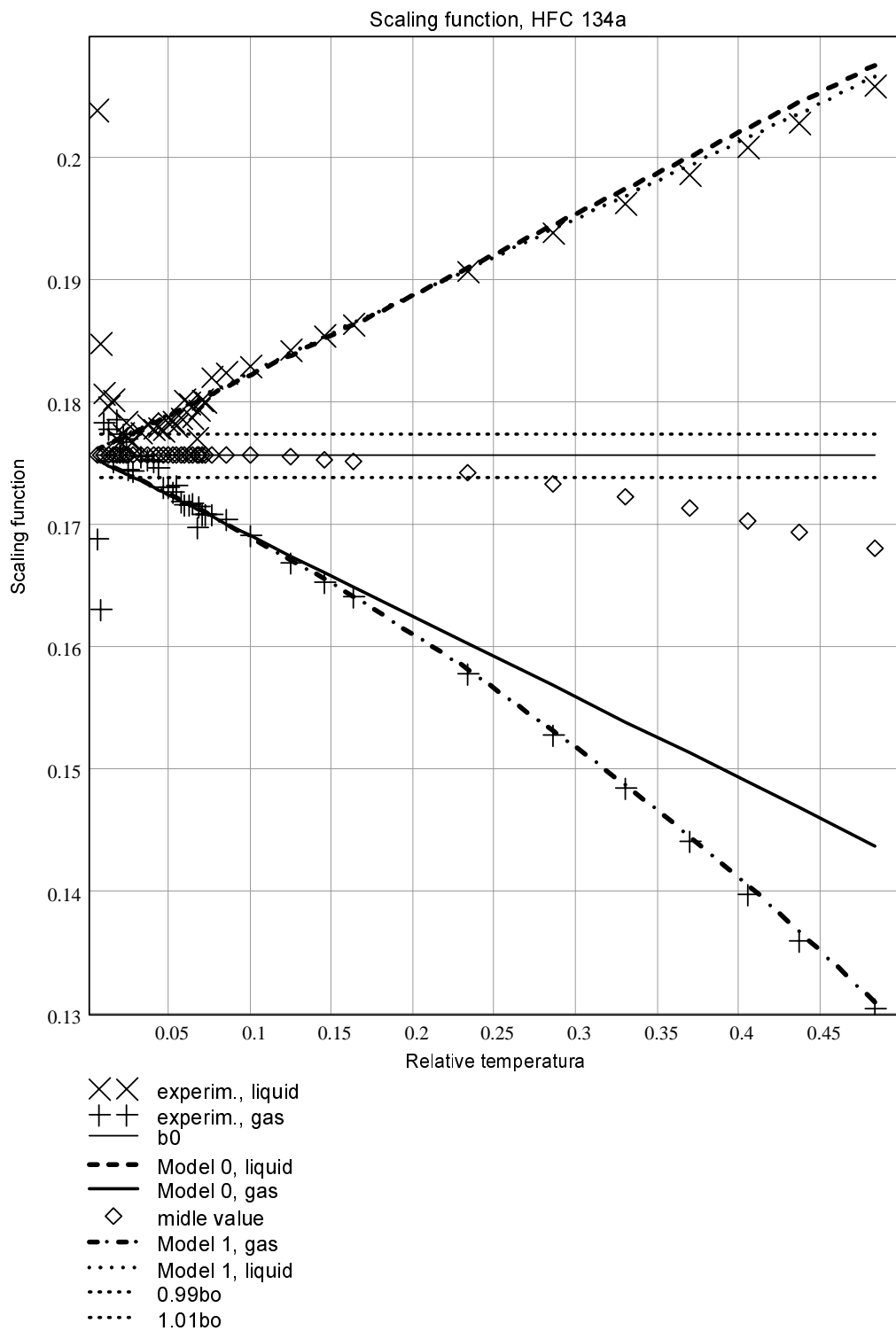
Fig. 2. The scaling functions  $\psi_{l,g}$  of HFC 134a.

Values are determined from 1) the experimental data, 2) Models 2;

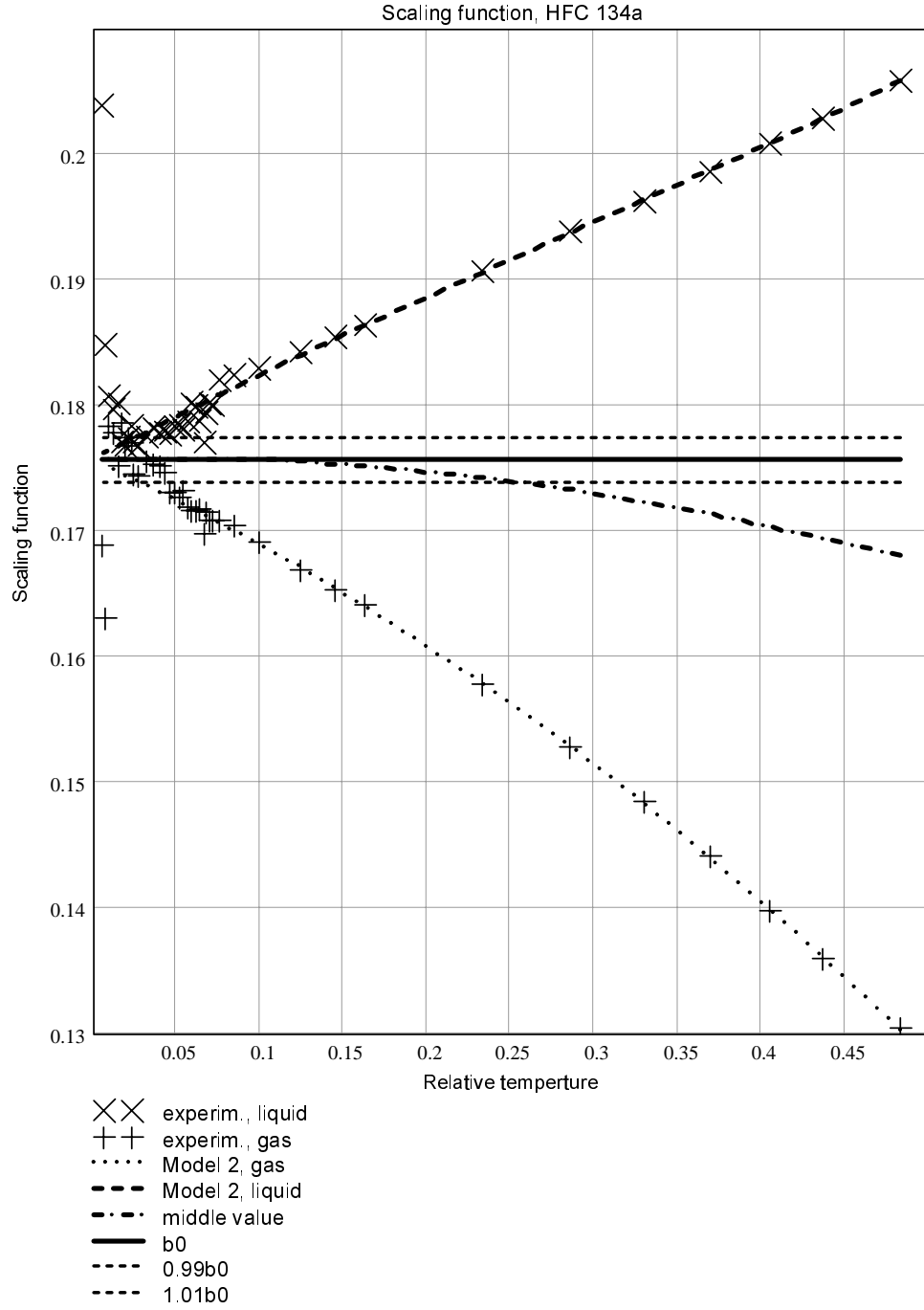
$b_0$  – leading amplitude  $B_{s0}$ ; relative temperature –  $\tau^{1-\alpha-\beta} = (1 - T/T_c)^{1-\alpha-\beta}$

Fig. 3. The influence of  $n_c$  on the criterions  $S_l$  for Model 1 and Model 2 of HFC 134a

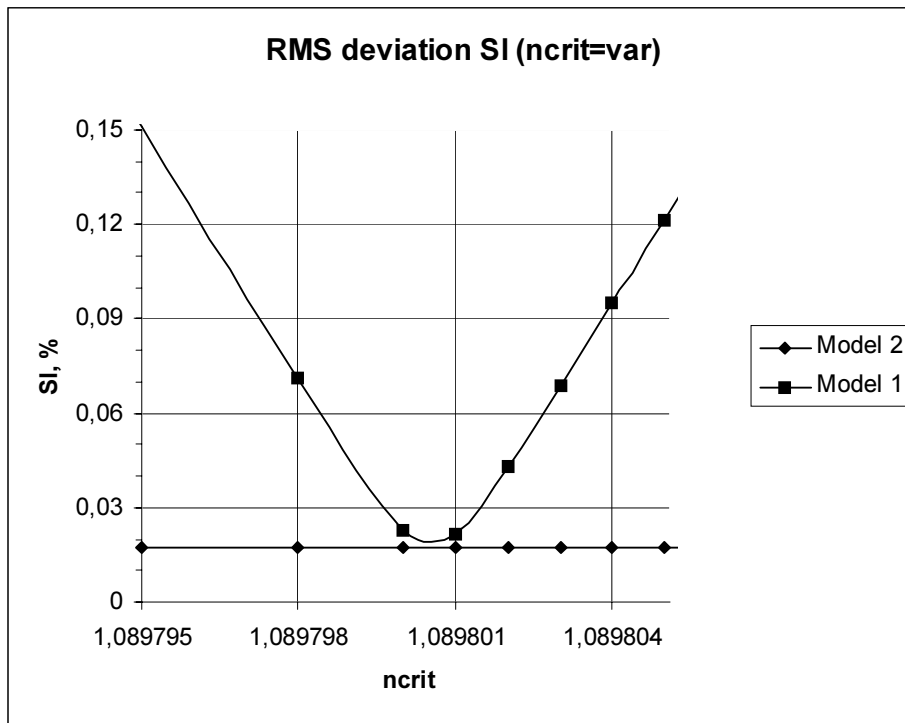
Fig. 4. The influence of  $T_c$  [K] on the criterions  $S_l$  for Model 1 and Model 2 of HFC 134a



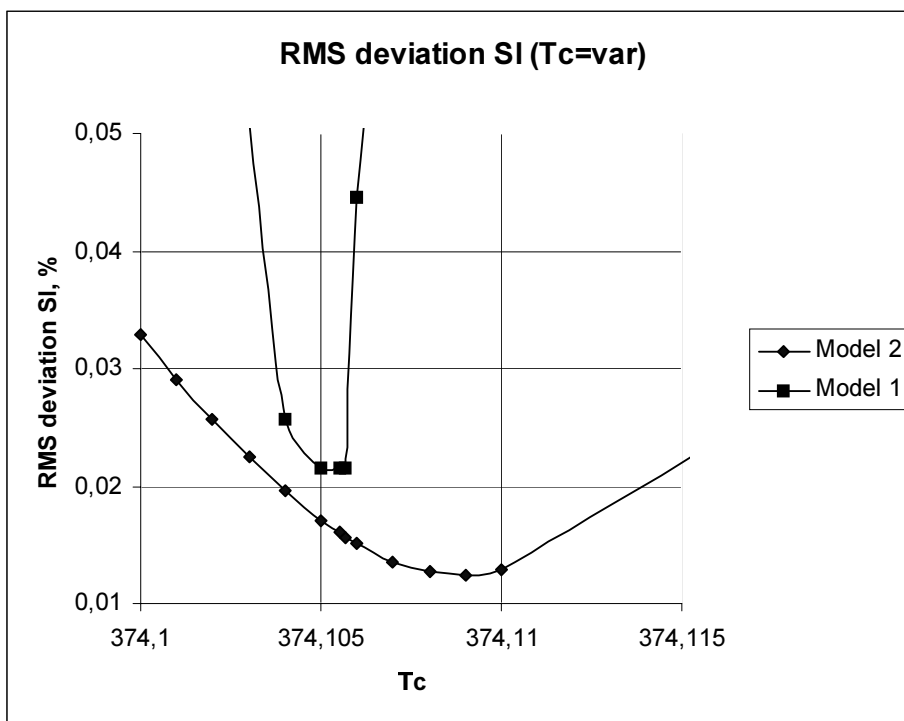
**Fig. 1.** The scaling functions  $\psi_{l,g}$  of HFC 134a.  
 Values are determined from 1) the experimental data, 2) Models 0,1;  
 $b0$  – leading amplitude  $B_{s0}$ ; relative temperature –  $\tau^{1-\alpha-\beta} = (1 - T/T_c)^{1-\alpha-\beta}$



**Fig. 2.** The scaling functions  $\psi_{l,g}$  of HFC 134a.  
 Values are determined from 1) the experimental data, 2) Models 2;  
 $b0$  – leading amplitude  $B_{s0}$ ; relative temperature –  $\tau^{1-\alpha-\beta} = (1 - T/T_c)^{1-\alpha-\beta}$



**Fig. 3.**



**Fig. 4.** The influence of  $T_c$  on the criterions  $S_l$  for Model 1 and Model 2